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# The Cell Method: an Enriched Description of Physics Starting from the Algebraic Formulation

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**Abstract:** In several recent papers studying the Cell Method (CM), which is a 5 numerical method based on a truly algebraic formulation, it has been shown that 6 numerical modeling in physics can be achieved even without starting from differ-7 ential equations, by using a direct algebraic formulation. In the present paper, our 8 focus will be above all on highlighting some of the theoretical features of this alq gebraic formulation to show that the CM is not simply a new numerical method 10 among many others, but a powerful numerical instrument that can be used to avoid 11 spurious solutions in computational physics. 12

Keywords: Algebraic Formulation, Differential Formulation, Cell Method, Spu rious Solutions, Nonlocality.

### 15 **1 Introduction**

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From the onset of differential calculus, over three centuries ago [Newton (1687)], 16 we have become accustomed to providing a differential formulation to each exper-17 imental law. Infinitesimal analysis has without doubt played a major role in the 18 mathematical treatment of physics in the past, and will continue to do so in the 19 future, but we must also be aware that, in using it, several important aspects of 20 the phenomenon being described, such as its geometrical and topological features 21 [Tonti (in press)], remain hidden. Moreover, applying the limit process introduces 22 some limitations as regularity conditions must be imposed on the field variables. 23 These regularity conditions, in particular those concerning differentiability, are the 24 price we pay for using a formalism that is both very advanced and easy to manipu-25 late. 26

Since the arrival of computers, differential equations have been discretized using
 one of various discretization methods (the finite element method FEM, the bound-

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CMC, vol.1, no.1, pp.1-23, 2013

ary element method BEM, the finite volume method FVM, the finite difference 29 method FDM, etc.), since the numerical solution, which is no longer an exact so-30 lution, cannot be achieved for the most general case if a system of algebraic phys-31 ical laws is not provided. Nevertheless, the very need to discretize the differential 32 equations, in order to achieve a numerical solution, gives rise to the question of 33 whether or not it is possible to formulate physical laws in an algebraic manner di-34 rectly, through a direct algebraic formulation. We will see, in this paper, that this is 35 possible and that a truly algebraic numerical method, the Cell Method (CM [Tonti 36 (2001)]), besides being physically more appealing, also allows us to avoid some of 37 the typical numerical problems of differential formulation, since it would appear 38 that many numerical problems are purely the result of the generally consolidated 39 custom of formulating the problem in differential form. 40

# 41 **2** Basics of algebraic formulation

The starting point in algebraic formulation [Tonti (1998); Tonti (2001); Freschi, Giaccone, and Repetto (2008); Alotto, Freschi, and Repetto (2010); Alotto, Freschi, Repetto, and Rosso (2013)] is that only a few physical variables arise directly as functions of points and instants. Most of them are obtained by performing densities and rates on variables related to extended space elements and time intervals.

47 We will call:

- global variable in space, a variable that is not the line, surface or volume density of another variable;
- 50
- global variable in time, a variable that is not the rate of another variable.

# 51 2.1 Global variables and their features

Global variables are essential to the philosophy of the Cell Method, since, by using these variables, it is possible to obtain an algebraic formulation directly and, what is most important, the global variables involved in obtaining the formulation do not have to be differentiable functions. Therefore, by using the limit process on the mean densities and rates of the global variables, we can obtain the traditional field functions of the differential formulation.

The main difference between the two formulations – algebraic and differential – lies precisely in the fact that the limit process is used in the latter. In effect, since calculating the densities and rates of the domain variables is based on the assumption that global variables are continuous and differentiable, the range of applicability of differential formulation is restricted to regions without material discontinuities or concentrated sources, while that of the algebraic formulation is not restricted

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to such regions [Ferretti (2004a,b); Ferretti, Casadio, and Di Leo (2008); Ferretti (2013)].

<sup>66</sup> Among the possible classifications of physical variables, the one we will adopt in

<sup>67</sup> this work makes the distinction between:

- configuration variables, which describe the field configuration;
- source variables, which describe the field sources.

Displacements in solid mechanics, velocity in fluid dynamics, electric potential in electrostatics and temperature in thermal conduction are all examples of configuration variables, while forces in solid mechanics and fluid dynamics, masses in geodesy, electric charges in electrostatics, electric currents in magnetostatics and heat in thermal conduction are instead examples of source variables.

75 The equations used to relate the configuration variables of the same physical theory

<sup>76</sup> to each other and the source variables of the same physical theory to each other

are known as topological equations, while those that relate configuration to source

variables, of the same physical theory, are known as constitutive equations.

Since each physical phenomenon occurs in space, and space has a multi-dimensional 79 geometrical structure, the physical variables themselves have a multi-dimensional 80 geometrical content. As a consequence, each of the global physical variables is 81 associated with one of the four space elements: point (P), line (L), surface (S) or 82 volume (V). The association between physical variables and space elements in di-83 mensions 0, 1, 2 and 3 is ignored in differential formulation, while it is emphasized 84 in the Cell Method, where it becomes the corner stone for building the relative 85 governing equations. As we will see better later, the fact that the Cell Method 86 takes account of the association between physical variables and space elements is 87 also the main reason why it does not present the spurious solutions of differen-88 tial formulation [Pimprikar, Teresa, Roy, Vasu, and Rajan (2013); Oian, Han, and 89 Atluri (2013); Kakuda, Nagashima, Hayashi, Obara, Toyotani, Katsurada, Higuchi, 90 and Matsuda (2012); Kakuda, Obara, Toyotani, Meguro, and Furuichi (2012); Cai, 91 Tian, and Atluri (2011); Chang (2011); Dong and Atluri (2011); Liu (2012); Jarak 92 and Sori\'c, (2011); Liu and Atluri (2011); Liu, Dai, and Atluri (2011); Wu and 93 Chang (2011); Cai, Paik, and Atluri (2010); Liu, Hong, and Atluri, (2010); Soares, 94 D. Jr. (2010); Yeih, Liu, Kuo, and Atluri (2010); Zhu, Cai, Paik, and Atluri (2010)]. 95 We will use algebraic topology notations to describe the four space elements P, L, 96 S and V. In algebraic topology, it is usual to consider cell-complexes, and to denote 97 the vertexes as 0-cells, the edges as 1-cells, the surfaces as 2-cells and the volumes 98

<sup>99</sup> as 3-cells (Fig. 1).

CMC, vol.1, no.1, pp.1-23, 2013



Figure 1: The four space elements in algebraic topology



Figure 2: Association between space elements and variables in continuum mechanics



Figure 3: Faces of a *p*-cell of degree 1, 2 and 3.

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Figure 4: Cofaces of a *p*-cell of degree 0, 1 and 2.

In continuum mechanics, volume forces, which are source variables, are associated with 3-cells, since their geometrical referents are volumes (Fig. 2). Analogously, for surface forces, which are source variables, the geometrical referents (the surfaces) are 2-cells; for strains, which are configuration variables, the geometrical referents (the lines) are 1-cells; and for displacements, which are configuration variables, the geometrical referents (the points) are 0-cells.

Algebraic topology also involves the notions of face and coface. If we consider a cell-complex made of *p*-cells of degree 0, 1, 2 and 3, the (p-1)-cells that bound a given *p*-cell are the faces of the *p*-cell (Fig. 3). The set of faces of a *p*-cell defines the boundary of the *p*-cell.

The (p+1)-cells that have a given *p*-cell as a common face are the cofaces of that *p*-cell (Fig. 4). The set of cofaces of a *p*-cell defines the coboundary of the *p*-cell.

# 112 2.2 How the Cell Method works

The Cell Method has often been compared to the Direct or Physical Approach, ini-113 tially used in the Finite Element Method [Huebner (1975); Livesley (1983); Fenner 114 (1996)], or to the Finite Volume Method and the Finite Difference Method. In par-115 ticular, the Cell Method may seem very similar to the vertex-based scheme of the 116 FVM [Mavripilis (1995)]. However, on deeper analysis of the similarities and dif-117 ferences between the CM and other discrete methods, the CM is shown to be based 118 on a new philosophy, where, for the moment, the CM is seen as the only truly alge-119 braic method. In effect, the key point to bear in mind in building a truly algebraic 120 formulation is that all operators must be discrete and use of the limit process must 121 be avoided at each level of the formulation. The direct or physical approach is not 122 suited to this, since it starts from the point-wise conservation equations of differen-123 tial formulation (Fig. 5) and, for differential formulation, there is the need for field 124 functions, which depend on the point position and the instant value. If the field 125 functions are not described directly in terms of point position and instant values, 126

CMC, vol.1, no.1, pp.1-23, 2013

they can be obtained by calculating the densities and rates of the global variables,
which are domain variables and depend on the point position and the instant value,
and also on line extensions, areas, volumes and time intervals.



Figure 5: Building an algebraic formulation through the Direct or Physical Approach, the Finite Volume Method, the Finite Difference Method and the Cell Method

- The space distribution of the point-wise field functions requires the introduction of coordinate systems (Fig. 5), whose purpose is to create a correspondence between the points of the space and the numbers, that is, their coordinates. This allows us to
- 133 describe geometry through mathematics.
- The algebraic formulation can be derived from the differential formulation through an integration process (Fig. 5) that is needed because, while in differential formula-
- tion geometry must be eliminated from the physical laws, in the numerical solution
- 137 geometry is essential.
- 138 The Finite Volume Method and the Finite Difference Method are also based on a
- differential formulation (Fig. 5). The Cell Method, on the contrary, uses global
- variables and balance equations in a global form. As a consequence, the relative
- <sup>141</sup> governing equations are expressed directly in algebraic form.

The CM uses cell-complexes (Fig. 5), which are the generalization of the coordi-142 nate systems to the algebraic formulation. The CM cell-complexes are not actually 143 the result of a domain discretization, a process needed in numerical analysis, as in 144 the case of the FEM. They are required in algebraic formulation, since global vari-145 ables are associated not only with points, as for differential formulation, but also 146 with lines, surfaces and volumes. In the CM, global variables are described directly 147 as they will be associated with the related space elements of the cell-complexes. 148 Consequently, in the algebraic formulation of physics, cell complexes have the 149 same role that coordinate systems have in differential formulation. Physical no-150 tions are therefore translated into mathematical notions through the intermediation 151 of topology and geometry. 152

The geometrical structure of space is very rich in algebraic formulation. It is possible, for example, to define an inner orientation for the elements in dimension 0, 1, 2 and 3 of a cell-complex (Fig. 5), which we call the primal cell-complex. Then, by considering the planes that are equidistant from the primal nodes, we can define a second cell complex (Fig. 5), called the dual cell-complex, which turns out to be provided with an outer orientation.

- Moreover, if we consider a time axis and subdivide a given time interval into many adjacent small time intervals (Fig. 5), we have a primal cell complex in time. In order to build the dual cell complex in time, we will consider the middle instant of each time interval. The result is that, similarly for the space elements, the primal and dual time elements are also provided with inner and outer orientation.
- We will now see how the space elements of the primal and dual cell-complexes 164 are strictly associated with global variables. For the example, in Fig. 6, on a two-165 dimensional domain, once a mesh has been introduced, it is natural to associate the 166 primal nodes with the displacements of the primal nodes and the total load over 167 an area surrounding the primal nodes, which is an area of the dual cell complex. 168 It follows that the displacements, which are configuration variables, are computed 169 on objects of the primal mesh, while the loads, which are source variables, are 170 computed on objects of the dual complex. 171
- This result is general, independently of the kind of configuration or source variable, the shape of the domain, or the physical theory involved. In effect, for each set of primal nodes and for each given physical theory, the source variables are always associated with the elements of the dual cell-complex and the configuration variables are always associated with the elements of the primal cell-complex (Fig. 7).
- The association of physical variables with the elements of a cell complex and its dual was first introduced by Okada and Onodera (1951) and Branin (1966). In the CM, the strong coupling between physical variables and oriented space elements

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8

Figure 6: Association between global variables and elements of the two cell complexes



Figure 7: Association between global variables and space elements of the primal and dual cell complexes, in different physical theories

180 becomes the key to giving a direct discrete formulation to physical laws.

Moreover, the existence of an underlying structure, common to different physical theories, is mainly responsible for the structural similarities presented in physical theories, commonly called "analogies". Today, we are able to explain these analogies in the light of the association between the global variables and the four space elements, since the homologous global variables of two physical theories are those associated to the same space element. In other words, the analogies between physical theories arise from the geometrical structure of the global variables and not

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from the similarity of the equations that relate variables to each other in differentphysical theories [Tonti (in press)].

### **3** The structure of the governing equations in the CM

# 191 3.1 Nonlocality in algebraic and differential formulations

For the nodes of a dual cell-complex in plane domains, we can choose, for example,
the barycenters of a primal cell-complex made of triangles, a simplicial primal
mesh (Fig. 8).

Since even in plane domains the primal mesh has thickness, which is a unit thickness, the dual nodes are not in the same plane as the primal nodes and the two meshes are shifted along the thickness (Fig. 9).

This is similar to the relative position of staggered elements, a commonly used mathematical expedient to avoid spurious solutions in physics. In particular, in solid mechanics, imbricate elements [Bažant, Belytschko, and Chang (1984); Belytschko, Bažant, Hyun, and Chang (1986)] are examples of staggered elements used for regularizing material instability in strain-softening materials, both in oneand two-dimensional domains (Fig. 10).

As it is now clear that global physical variables are naturally associated with the space elements of the primal and dual cell-complexes, it therefore follows that staggering is not only a mathematical expedient used to regularize the solution [Stevens and Power (2010)], but is also necessary in physics to take account of the association between physical variables and oriented space elements.

In solid mechanics, staggering is used to provide the differential formulation with 209 nonlocal properties, when modeling heterogeneous materials. It is now the com-210 mon opinion that the classical local continuum concept, where stress at a given 211 point depends only on the deformation and temperature history at that precise point, 212 cannot adequately describe damage in heterogeneous materials by means of differ-213 ential formulation, particularly when size-effect is involved. Indeed, modeling the 214 size-effect is impossible in the context of classical plasticity, both in problems in-215 volving strain-softening [Duhem (1893); Krumhansl (1965); Rogula (1965); Erin-216 gen (1966); Kunin (1966); Kröner (1968)] and in those with no strain-softening at 217 all. 218

The first criticisms of the local approach date back to the 1960s [Krumhansl (1965), Rogula (1965), Eringen (1966), Kunin (1966) and Kröner (1968)] and are based on the microstructure of matter. In effect, all materials are characterized by microstructural details, with size ranging over several orders of magnitude [Bažant and Jirásek (2002)]. They cannot, therefore, be broken down into a set of infinites-

CMC, vol.1, no.1, pp.1-23, 2013



Figure 8: Primal and dual cell complexes in plane domains



Figure 9: Staggering of the primal and dual cell complexes along the thickness



Figure 10: Imbricate elements in one- and two-dimnsional domains

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imal volumes, each of which can be described independently. Consequently, the idea was advanced that heterogeneous materials should be modeled properly by some kind of nonlocal continuum [Duhem (1893)], in which the stress at a certain point is a function of the strain distribution over a certain representative volume centered at that point [Bažant and Chang (1984)]. This idea led to models where the classical continuum description is improved by introducing an internal length parameter into the constitutive laws.

According to the mathematical definition of nonlocality in the narrow sense, given by Rogula, the operator *A* in the abstract form of the fundamental equations of any physical theory:

$$Au = f, (1)$$

is called local when, if u(x) = v(x) for all x in a neighborhood of point  $x_0$ , then 231 Au(x) = Av(x). Bažant and Jirásek (2002) and Ferretti (2005) pointed out that the 232 differential operators satisfy this condition, because the derivatives of any arbitrary 233 order do not change if the differentiated function only changes outside the small 234 neighborhood of the point where the derivatives are taken, and, consequently, the 235 differential operators are local. It follows that any formulation using differential 236 operators is intrinsically local. That is, differential formulation is not adequate for 237 describing nonlocal effects. 238



Figure 11: Losing and reintroducing metrics in the differential formulation

In the light of the former discussion on the geometrical content of global variables,
we can now provide an alternative interpretation of nonlocality. As we have discussed previously, the reason why differential operators are local in nature lies in

CMC, vol.1, no.1, pp.1-23, 2013

the use of the limit process. The density-finding process is carried out with the intention of formulating the field laws in an exact form. However, differential formulation can be solved only for very simple geometries and under particular boundary conditions (Fig. 11). Moreover, with the global variables being reduced to point and instant variables, we can no longer describe more than 0-dimensional effects, that is, the nonlocal effects. Metrics must be reintroduced a-posteriori in the discretization process, if we want to model nonlocality (Fig. 11).

We may now ask where the length scale is to be reintroduced. In nonlocal ap-249 proaches, a length scale is incorporated into the constitutive laws, but there is no 250 evidence that this choice is the only one, or even the most appealing from a physi-251 cal point of view. On the contrary, we have seen that the physical global variables 252 themselves have a multi-dimensional geometrical content. It therefore seems that 253 dimensional scales and nonlocal effects are directly associated with global vari-254 ables, and nonlocality seems to be a property of global variables, not a preroga-255 tive of constitutive laws. Consequently, reintroducing or preserving nonlocality in 256 governing equations is physically more correct than reintroducing nonlocality into 257 constitutive equations. When speaking of reintroduction, we are dealing with dif-258 ferential formulation, while, when speaking of preservation, we are dealing with 259 algebraic formulation. The difference is not negligible, since, in order to rein-260 troduce a length scale, a suitable approach must be developed, while, in order to 261 preserve the length scales, it is sufficient to avoid the limit process and, by using an 262 algebraic approach, a nonlocal formulation is automatically obtained. 263

Besides this, due to the structure of the discrete operators, even the topological equations are provided with nonlocal properties in algebraic formulation. The reason for this lies in the relationship between the discrete p-forms of different degrees.

### 268 3.2 The discrete p-forms (cochains)

A physical variable  $\phi$  associated with one set of *p*-cells of a cell-complex defines a discrete *p*-form (or a discrete form of degree *p*). The potential of a vector field, line integral of a vector, flux and mass content are discrete forms of degree 0, 1, 2 and 3, respectively (Tab. 1).

Variable	Potential of a	Line integral of	Flux	Mass content
	vector field	a vector		
Evaluated on	0-cells (points)	1-cells (lines)	2-cells (surfaces)	3-cells (volumes)
Discrete <i>p</i> -form	discrete 0-form	discrete 1-form	discrete 2-form	discrete 3-form

Table 1: Examples of discrete *p*-forms

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The discrete *p*-forms generalize the notion of field functions, because, in a discrete *p*-form  $\Phi[S]$ , we associate the value of a physical variable to the space elements of degree *p*, while the field functions f(P) always associate the value of a physical variable to the points of the domain. As a consequence,  $\Phi[S]$  is a set function, while f(P) is a point function.

The notion of discrete form is the discrete version of the exterior differential form, a mathematical formalism that has the great merit of highlighting the geometrical background of physical variables, something ignored by differential calculus, providing a description that is independent of the coordinate system used. Nevertheless, this formalism uses field variables instead of global variables and, for this reason, it must use the notion of derivative.

# 284 3.3 The coboundary process and its implications on nonlocality

The coboundary process on a discrete *p*-form is a process that generates a discrete (*p*+1)-form. It is worth noting that balance, circuital equations, and equations forming differences can be expressed by the coboundary process performed on discrete *p*-forms of degree 2, 1, 0, respectively. Thus, the coboundary process plays a key role in physics.

This process is analogous, in an algebraic setting, to the exterior differentiation on exterior differential forms and leads to discrete operators, whose elements are the incidence numbers, equal to 0, +1, or -1. In particular, the incidence number of a p-cell with a (p-1)-cell is equal to:

- 0, if the (p-1)-cell is not on the boundary of the *p*-cell;
- +1, if the (p-1)-cell is on the boundary of the *p*-cell and the orientations of the *p*-cell and (p-1)-cell are compatible (Fig. 12);
- -1, if the (p-1)-cell is on the boundary of the *p*-cell and the orientations of the *p*-cell and (p-1)-cell are not compatible (Fig. 13).
- <sup>299</sup> In a three-dimensional space, we can define three incidence matrices:
- **G**: matrix of the incidence numbers between 1-cells and 0-cells;
- C: matrix of the incidence numbers between 2-cells and 1-cells;
- **D**: matrix of the incidence numbers between 3-cells and 2-cells.

The incidence matrices **G**, **C**, and **D** are the discrete versions of the differential operators "grad", "curl", and "div", respectively.

The coboundary process on a discrete *p*-form,  $\Phi^p$ , is performed in two steps:

CMC, vol.1, no.1, pp.1-23, 2013



Figure 13: Incidence numbers equal to -1

- 1. For each *p*-cell: we assign the value  $\phi_n^p$ , evaluated on the *nth p*-cell, to each coface (of degree *p*+1) of the *nth p*-cell, with the plus or minus sign according to the mutual incidence number;
- 2. For each (p+1)-cell: we sum the values  $\phi_{1,2,\dots,h}^p$  coming from all the faces (of degree *p*) of the boundary.
- At the end of the process, we obtain a discrete (p+1)-form.

14

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- The consequence of this two-step process, when we enforce balance in the CM, which is a coboundary process on a discrete p-form of degree 2, the flux, described as follows:
- first step (on each 2-cell): transfer the fluxes associated with all 2-cells to their cofaces, each multiplied by the relative incidence number;

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317 318 • second step (on each 3-cell): perform the algebraic sum of the fluxes coming from the first step;

is that the global source variables involved in the balance of one 3-cell are also 319 involved in the balance of all the surrounding 3-cells. This happens since each 3-320 cell is common to more than one 2-cell. Consequently, the balance at a given 3-cell 321 does not depend on the current values, or previous history, of the global source 322 variables at that 3-cell only, but on the current values, and previous history, taken 323 by the global source variables in all the surrounding 3-cells. This gives nonlocal 324 properties to the balance equations of the algebraic formulation, while the balance 325 equations of the differential formulation are local. 326

Achieving nonlocality in the CM balance equations is very important, as it enriches the description of physics given by the CM, compared to the descriptions given by any other numerical method, even those known as discrete methods. This enrichment follows on from the structure of the coboundary process given to the balance equations and from more than one 2-cell sharing the same 3-cell. That is, it is a consequence of the structure of the balance equations, and there is no need to modify the balance equations in any way to provide them with nonlocal properties.

Moreover, coboundary processes on discrete p-forms defined on configuration vari-334 ables generate discrete (p+1)-forms defined on configuration variables, and cobound-335 ary processes on discrete p-forms defined on source variables generate discrete 336 (p+1)-forms defined on source variables. Thus, the coboundary process creates 337 a relationship between different degrees of discrete forms of the same kind of 338 variable. This means that all the topological equations are coboundary processes 339 [Ferretti (in press)], and therefore, even enforcing compatibility in the CM is a 340 coboundary process. As a consequence, even the Kinematic equations are pro-341 vided with nonlocal properties in the CM, while the Kinematic equations of the 342 differential formulation are local. We can therefore conclude that all the governing 343 equations of the algebraic formulation are nonlocal: constitutive relationships are 344 nonlocal due to the staggering between the elements of the primal cell complex, on 345 which we compute configuration variables, and the dual cell complex, on which we 346 compute source variables, while the balance and Kinematic equations are nonlocal, 347 since they are the results of coboundary processes. This means that obtaining a 348 nonlocal formulation by using discrete operators is possible, besides being physi-349 cally appealing. The new nonlocal formulation is desirable from a numerical point 350 of view, since the numerical solution is reached sooner using discrete operators 351 than with differential operators. 352

### 353 3.4 Implementation of the equations

The CM equations are implemented in the same manner as for FEM. The linear interpolation of the CM for solid mechanics in two-dimensional domains was provided in Ferretti (2003a), with a Kinematic equation for each primal cell:

$$\boldsymbol{\varepsilon} = \boldsymbol{B}\boldsymbol{u},\tag{2}$$

$$\boldsymbol{u} = \begin{bmatrix} w_k & v_k & w_i & v_i & w_j & v_j \end{bmatrix}^T,$$
(3)

$$\boldsymbol{B} = \frac{1}{\Delta_{ijk}} \begin{bmatrix} \Delta y_{ji} & 0 & \Delta y_{kj} & 0 & \Delta y_{ik} & 0\\ 0 & \Delta x_{ij} & 0 & \Delta x_{jk} & 0 & \Delta x_{ki}\\ \Delta x_{ij} & \Delta y_{ji} & \Delta x_{jk} & \Delta y_{kj} & \Delta x_{ki} & \Delta y_{ik} \end{bmatrix}.$$
(4)

a constitutive law:

$$\boldsymbol{\sigma} = \boldsymbol{D}\boldsymbol{\varepsilon}.$$
 (5)

and an equilibrium equation for each dual cell (Fig. 14):

$$\sum_{i} \boldsymbol{Q}_{kj} + \boldsymbol{F}_{k} = 0, \tag{6}$$

$$\boldsymbol{Q} = \boldsymbol{N}\boldsymbol{\sigma} = \boldsymbol{N}\boldsymbol{D}\boldsymbol{\varepsilon} = (\boldsymbol{N}\boldsymbol{D}\boldsymbol{B})\boldsymbol{u},\tag{7}$$

$$\boldsymbol{N} = \begin{bmatrix} S_x & 0 & S_y \\ 0 & S_y & S_x \end{bmatrix},\tag{8}$$

$$\boldsymbol{S} = \boldsymbol{R}\boldsymbol{L}.$$

The linear system of equations can be written in the form:

$$\boldsymbol{F} = \boldsymbol{K}\boldsymbol{U},\tag{10}$$

where F and U are the force and displacement vectors, respectively, and K is analogous to the FEM stiffness matrix, which is symmetric and defined as positive for properly constrained systems.

The CM was also implemented for solid mechanics with quadratic interpolation of

the displacements in two-dimensional domains [Cosmi (2000)] and three-dimensional domains [Pani and Taddei (2013)].

Lastly, Zovatto (2001) proposed a meshfree approach of the CM, including for three-dimensional domains. Meshfree and meshless approaches are very useful in problems of fracture mechanics where the crack being studied is simulated as a discontinuity of the displacement field. In effect, crack geometry updating and remeshing on the whole domain is a very expensive process from a computational



Figure 14: Primal and dual meshes for CM analysis in two-dimensional domains

point of view. Some of the most recent achievements for the CM meshless approach can be found in Pani and Taddei (2013) and Taddei, Pani, Zovatto, Tonti,
and Viceconti (2008).

As far as the convergence rate is concerned, it has been shown [Tonti (2001)] that this depends on the choice of dual polygons. The most convenient choice, giving a convergence rate equal to four [Cosmi (2000)], is to use Gauss points to build the dual polygons.

# 372 4 Conclusions

In the present paper, we have discussed where the Cell Method stands in respect 373 to the discussion on local or nonlocal descriptions of the continuum for modeling 374 heterogeneous brittle materials. We have found that the CM can provide a direct 375 nonlocal description of the continuum, without requiring any sort of enrichment to 376 the constitutive laws, by means of length scales, as is usually the case for nonlocal 377 approaches in solid mechanics. In particular, we can state that the CM does not pro-378 vide an enriched continuum description only as far as the constitutive relationships 379 are concerned. It enriches all the governing equations involved in the physical the-380 ory in a very simple manner, by simply taking account of the association between 381 global variables and extended space elements. The consequence is that, by using 382 the CM, there is no need to recover nonlocality a-posteriori, as for differential for-383 mulation. Nonlocality is - we could say - intrinsic to algebraic formulation and is 384 the result of using global instead of field variables, something that distinguishes the 385 cell method from any other numerical method, at the moment. 386

17

CMC, vol.1, no.1, pp.1-23, 2013

As already discussed in Ferretti [2005], it is worth noting that, in the first theories 387 of nonlocal elasticity developed by Eringen and Edelen [Eringen (1966); Edelen et 388 al. (1971); Eringen (1972); Eringen and Edelen (1972)], nonlocality was a property 389 of the elastic problem in its complex, and not solely of its constitutive relationships. 390 In other words, in these nonlocality theories, there was already the idea that non-391 locality is a property of the governing equations. Nevertheless, this idea was not 392 developed further, since the theories of nonlocal elasticity were too complicated to 393 be calibrated and verified experimentally, let alone to be applied to any real prob-394 lems [Bažant and Jirásek (2002)]. Treating only the stress-strain relationships as 395 nonlocal, while the equilibrium and kinematic equations and their corresponding 396 boundary conditions retain their standard form, was something needed later [Erin-397 gen and Kim (1974); Eringen et al. (1977)], to provide a practical formulation of 398 these early theories. Consequently, incorporating the length scale into the constitu-399 tive relationships only is the practical simplification of a more general theory and 400 has no evident justification from a physical point of view. In this sense, we can 401 state that the cell method provides a physically more appealing nonlocal formu-402 lation when compared to nonlocal differential approaches. Ferretti provides sev-403 eral numerical results [Ferretti (2012), Ferretti (2005), Ferretti (2004c) and Ferretti 404 (2003b)] showing how the CM, together with a new local constitutive law for het-405 erogeneous brittle materials - the effective law [Ferretti (2004d); Ferretti (2004e); 406 Ferretti (2004f); Ferretti and Di Leo (2008)] - actually offers a nonlocal descrip-407 tion for solid mechanics, allowing us to model the size- and shape-effects, which is 408 impossible in local differential approaches. 409

A properly formulated enriched classical continuum for the differential formulation 410 has a regularizing effect when modeling strain-softening materials, because it acts 411 as a localization limiter, so that the boundary value problem is once again well-412 posed. Boundary value problems with strain-softening constitutive models that are 413 ill-posed are just some of the many examples of spurious solutions for differential 414 formulation. Since the CM is a multidisciplinary method, the intrinsic nonlocality 415 of the CM governing equations means that we can assume that, using the CM, 416 spurious solutions can be avoided whenever they appear in differential formulation, 417 independently of the physical theory involved. This is the really strong point for 418 the CM, setting it apart from all other numerical methods, for the moment. 419

In conclusion, the Cell Method enriches the computational description of physics
by using notions of algebraic topology, as well as of mathematics. The result is
twofold:

• The Cell Method provides the physical laws in an algebraic manner, directly, avoiding the use of any discretization procedure.

- 19
- The Cell Method is tantamount to abandoning the principle of local action, therefore of avoiding the spurious solutions of differential formulation.

### 427 **References**

- Alotto, P.; Freschi, F.; Repetto, M. (2010): Multiphysics problems via the cell
  method: The role of Tonti diagrams. *IEEE Transactions on Magnetics*, vol. 46, no.
  8, pp. 2959–2962.
- Alotto, P.; Freschi, F.; Repetto, M.; Rosso, C. (2013): The Cell Method for Elec-
- trical Engineering and Multiphysics Problems An Introduction. Lecture Notes in
   Electrical Engineering, Springer.
- **Bažant, Z. P.; Chang, T.P.** (1984): Is Strain-Softening Mathematically Admissible? *Proc.*, 5<sup>th</sup> Engineering Mechanics Division, vol. 2, pp. 1377–1380.
- Bažant, Z. P.; Belytschko, T. B.; Chang, T.P. (1984): Continuum Model for Strain
  Softening. J. Eng. Mech., vol. 110, no. 12, pp. 1666–1692.
- **Bažant, Z. P.; Jirásek, M.** (2002): Nonlocal Integral Formulations of Plasticity and Damage: Survey of Progress. *J. Eng. Mech.*, vol. 128, no. 11, pp. 1119–1149.
- Belytschko, T.; Bažant, Z. P.; Hyun, Y.-W.; Chang, T.-P. (1986): Strain Soften-
- ing Materials and Finite-Element Solutions. *Comput. Struct.*, vol. 23, pp. 163–180.
- Belytschko, T.; Krongauz, Y.; Organ, D.; Fleming, M.; Krysl, P. (1996): Meshless Methods: an Overview and Recent Developments. *Computer Methods Appl. Mech Engrg.*, vol. 139, pp 3–47.
- Branin, F. H. Jr. (1966): The Algebraic Topological Basis for Network Analogies
  and the Vector Calculus. *Proc., Symp. on Generalized Networks*, Brooklyn Polit.,
  pp. 453–487.
- 448 Cai, Y.C.; Paik, J.K.; Atluri, S.N. (2010): Locking-free thick-thin rod/beam ele-
- ment for large deformation analyses of space-frame structures, based on the reissner variational principle and a von karman type nonlinear theory. *CMES: Comput.*
- <sup>451</sup> *Model. Eng. Sci.*, vol. 58, no. 1, pp. 75-108.
- Cai, Y.C.; Tian, L.G.; Atluri, S.N. (2011): A simple locking-free discrete shear
  triangular plate element. *CMES: Comput. Model. Eng. Sci.*, vol. 77, no. 3-4, pp.
  221-238.
- 455 Chang C.-W. (2011): A New Quasi-Boundary Scheme for Three-Dimensional
- <sup>456</sup> Backward Heat Conduction Problems. *CMC: Comput. Mater. Con.*, vol. 24, <sup>457</sup> no. 3, pp. 209–238.
- **Cosmi, F.** (2000): Applicazione del Metodo delle Celle con Approssimazione Quadratica. *Proc.*, *AIAS 2000*, Lucca, Italy, pp. 131–140.
- 460 Dong, L.; Atluri, S.N. (2011): A simple procedure to develop efficient & stable

- <sup>461</sup> hybrid/mixed elements, and Voronoi cell finite elements for macro- & microme-<sup>462</sup> chanics. *CMC: Comput. Mater. Con.*, vol. 24, no. 1, pp. 61–104.
- <sup>463</sup> **Duhem, P.** (1893): Le Potentiel Thermodynamique et la Pression Hydrostatique.
- 464 Ann. Sci. Ecole Norm. S., vol. 10, pp. 183–230.
- **Edelen, D.G.B.; Green, A. E.; Laws, N.** (1971): Nonlocal Continuum Mechanics.
- 466 Arch. Ration. Mech. Anal., vol. 43, pp. 36–44.
- **Eringen, A.C.** (1966): A Unified Theory of Thermomechanical Materials. *Int. J Eng. Sci.*, vol. 4, pp. 179–202.
- 469 Eringen, A.C. (1972): Linear Theory of Nonlocal Elasticity and Dispersion of
- 470 Plane Waves. Int. J Eng. Sci., vol. 10, pp. 425–435.
- 471 Eringen, A.C.; Edelen, D. G. B. (1972): On Nonlocal Elasticity. Int. J Eng. Sci.,
- 472 vol. 10, pp. 233–248.
- **Eringen, A.C.; Kim, B. S.** (1974): Stress Concentration at the Tip of a Crack. *Mech. Res. Commun.*, vol. 1, pp. 233–237.
- 475 Eringen, A.C.; Speziale, C. G.; Kim, B. S. (1977): Crack-Tip Problem in Nonlo-
- 476 cal Elasticity. J. Mech. Phys. Solids, vol. 25, pp. 339–355.
- Fenner, R.T. (1996): *Finite Element Methods for Engineers*, Imperial College
  Press, London.
- 479 Ferretti, E. (2003a): Crack Propagation Modeling by Remeshing using the Cell
- 480 Method (CM). CMES: Comput. Model. Eng. Sci., vol. 4, no. 1, pp. 51–72.
- 481 Ferretti, E. (2003b): Modeling of Compressive Tests on FRP Wrapped Concrete
- 482 Cylinders trough a Novel Triaxial Concrete Constitutive Law. SITA: Scientific Is-
- *rael Technological Advantages*, vol. 5, pp. 20–43.
- 484 Ferretti, E. (2004a): Crack-Path Analysis for Brittle and Non-Brittle Cracks: a
- Cell Method Approach. *CMES: Comput. Model. Eng. Sci.*, vol. 6, no. 3, pp. 227-244.
- **Ferretti, E.** (2004b): A Cell Method (CM) Code for Modeling the Pullout Test
- 488 Step-Wise. CMES: Comput. Model. Eng. Sci., vol. 6, no. 5, pp. 453–476.
- **Ferretti, E.** (2004c): A Discrete Nonlocal Formulation using Local Constitutive Laws. *Int. J. Fracture*, vol. 130, no. 3, pp. L175–L182.
- 491 Ferretti, E. (2004d): A Discussion of Strain-Softening in Concrete. Int. J. Fracture
- <sup>492</sup> (Letters section), vol. 126, no. 1, pp. L3–L10.
- 493 Ferretti, E. (2004e): Experimental Procedure for Verifying Strain-Softening in
- <sup>494</sup> Concrete. Int. J. Fracture (Letters section), vol. 126, no. 2, pp. L27–L34.
- Ferretti, E. (2004f): On Poisson's Ratio and Volumetric Strain in Concrete. Int. J.
- 496 Fracture (Letters section), vol. 126, no. 3, pp. L49–L55.

- 497 Ferretti, E. (2005): A Local Strictly Nondecreasing Material Law for Modeling
- <sup>498</sup> Softening and Size-Effect: a Discrete Approach. CMES: Comput. Model. Eng.
- 499 Sci., vol. 9, no. 1, pp. 19–48.
- **Ferretti, E.** (2012): Shape-Effect in the Effective Law of Plain and Rubberized Concrete. *CMC: Comput. Mater. Con.*, vol. 30, no. 3, pp. 237–284.
- <sup>502</sup> Ferretti, E. (2013): A Cell Method Stress Analysis in Thin Floor Tiles Subjected
- <sup>503</sup> to Temperature Variation. Submitted to CMC: Comput. Mater. Con.
- **Ferretti, E.** (in press): The Cell Method: a Purely Algebraic Computational Method
- <sup>505</sup> in Physics and Engineering Science, *Momentum Press*.
- 506 Ferretti, E.; Casadio, E.; Di Leo, A. (2008): Masonry Walls under Shear Test: a
- <sup>507</sup> CM Modeling. CMES: Comput. Model. Eng. Sci., vol. 30, no. 3, pp 163–190.
- 508 Ferretti, E.; Di Leo, A. (2008): Cracking and Creep Role in Displacement at
- 509 Constant Load: Concrete Solids in Compression. CMC: Comput. Mater. Con.,
- <sup>510</sup> vol. 7, no. 2, pp. 59–80.
- 511 Freschi, F.; Giaccone, L.; Repetto, M. (2008): Educational value of the algebraic
- numerical methods in electromagnetism. COMPEL The International Journal for
- 513 Computation and Mathematics in Electrical and Electronic Engineering, vol. 27,
- <sup>514</sup> no. 6, pp. 1343–1357.
- Okada, S.; Onodera, R. (1951): Algebraification of Field Laws of Physics by
  Poincar Process. *Bull. of Yamagata University Natural Sciences*, vol. 1, no. 4,
  pp. 79–86.
- <sup>518</sup> Huebner, K. H. (1975): *The Finite Element Method for Engineers*, Wiley.
- 519 Kakuda, K.; Nagashima, T.; Hayashi, Y.; Obara, S.; Toyotani, J.; Katsurada,
- <sup>520</sup> N.; Higuchi, S.; Matsuda, S. (2012): Particle-based Fluid Flow Simulations on
- 521 GPGPU Using CUDA. CMES: Comput. Model. Eng. Sci., vol. 88, no. 1, pp
- 522 17–28.
- Jarak, T.; Sori\'c, J. (2011): On Shear Locking in MLPG Solid-Shell Approach.
- <sup>524</sup> CMES: Comput. Model. Eng. Sci., vol. 81, no. 2, pp 157–194.
- Kakuda, K.; Obara, S.; Toyotani, J.; Meguro, M.; Furuichi, M. (2012): Fluid
   Flow Simulation Using Particle Method and Its Physics-based Computer Graphics.
- 527 CMES: Comput. Model. Eng. Sci., vol. 83, no. 1, pp 57–72.
- **Kröner, E.** (1968): Elasticity Theory of Materials with Long-Range Cohesive Forces. *Int. J. Solids Struct.*, vol. 3, pp. 731–742.
- 530 Krumhansl, J. A. (1965): Generalized Continuum Field Representation for Lattice
- <sup>531</sup> Vibrations. In *Lattice dynamics*, R. F. Wallis ed., Pergamon, London, pp. 627–634.
- 532 Kunin, I. A. (1966): Theory of Elasticity with Spatial Dispersion. Prikl. Mat.

- 533 Mekh. (in Russian), vol. 30, pp. 866.
- Liu, C.-S. (2012): Optimally Generalized Regularization Methods for Solving Lin-
- ear Inverse Problems. CMC: Comput. Mater. Con., vol. 29, no. 2, pp. 103–128.
- Liu, C.-S.; Atluri, S.N. (2011): An iterative method using an optimal descent vector, for solving an Ill-conditioned system Bx = b, better and faster than the conjugate gradient method. *CMES: Comput. Model. Eng. Sci.*, vol. 80, no. 3-4, pp 275–298.
- Liu, C.-S.; Dai, H.-H.; Atluri, S.N. (2011): Iterative Solution of a System of Non-
- <sup>541</sup> linear Algebraic Equations F(x)=0, Using dot  $x=\lambda[\alpha R+\beta P]$  or dot  $x=\lambda[\alpha F+\beta P^*]$
- <sup>542</sup> **R** is a Normal to a Hyper-Surface Function of **F**, **P** Normal to **R**, and **P**\* Normal to
- 543 F. CMES: Comput. Model. Eng. Sci., vol. 81, no. 3, pp 335–363.
- Liu, C.-S.; Hong, H.-K.; Atluri, S.N. (2010): Novel algorithms based on the conjugate gradient method for inverting ill-conditioned matrices, and a new regularization method to solve ill-posed linear systems. *CMES: Comput. Model. Eng. Sci.*, vol. 60, no. 3, pp 279–308.
- Livesley, R. K. (1983): *Finite Elements, an Introduction for Engineers*, Cambridge
  University Press.
- <sup>550</sup> Mavripilis, D. J. (1995): Multigrid Techniques for Unstructured Meshes. Lecture,
- 551 Series 1995-02, Computational Fluid Dynamics, Von Karman Institute of Fluid
- 552 Dynamics.
- **Newton, I.** (1687): *Philosophiae Naturalis Principia Mathematica*.
- Pani, M.; Taddei, F. (2013): The Cell Method: Quadratic Interpolation with
  Tetraedra for 3D Scalar Fields. To appear in *CMES: Comput. Model. Eng. Sci.*
- <sup>556</sup> Pimprikar, N.; Teresa, J.; Roy, D.; Vasu, RM.; Rajan. K. (2013): An approx-
- <sup>557</sup> imately H<sup>1</sup>-optimal Petrov-Galerkin meshfree method: application to computation
- of scattered light for optical tomography. CMES: Comput. Model. Eng. Sci., vol.
- <sup>559</sup> 92, no. 1, pp. 33–61.
- <sup>560</sup> Qian, Z.Y.; Han, Z.D.; Atluri, S.N. (2013): A fast regularized boundary integral
- method for practical acoustic problems. *CMES: Comput. Model. Eng. Sci.*, vol. 91, no. 6, pp. 463–484.
- <sup>563</sup> Rogula, D. (1965): Influence of Spatial Acoustic Dispersion on Dynamical Prop-
- erties of Dislocations. I. Bulletin de l'Académie Polonaise des Sciences, Séries des Sciences Techniques, vol. 13, pp. 337–343.
- 566 Soares, D. Jr. (2010): A Time-Domain Meshless Local Petrov-Galerkin Formula-
- tion for the Dynamic Analysis of Nonlinear Porous Media. *CMES: Comput. Model*.
- 568 Eng. Sci., vol. 66, no. 3, pp. 227–248.
- 569 Stevens, D.; Power, W. (2010): A Scalable Meshless Formulation Based on RBF

- <sup>570</sup> Hermitian Interpolation for 3D Nonlinear Heat Conduction Problems. *CMES:* <sup>571</sup> *Comput. Model. Eng. Sci.*, vol. 55, no. 2, pp. 111–146.
- Taddei, F.; Pani, M.; Zovatto, L.; Tonti, E.; Viceconti, M. (2008): A New Mesh-
- <sup>573</sup> less Approach for Subject-Specific Strain Prediction in Long Bones: Evaluation of
- Accuracy. Clinical Biomechanics, vol. 23, no.9, pp. 1192–1199.
- 575 Tonti, E. (1998): Algebraic Topology and Computational Electromagnetism. Fourth
- 576 International Worksop on the Electric and Magnetic Field: from Numerical Models
- to industrial Applications, Marseille, 284-294.
- **Tonti, E.** (2001): A Direct Discrete Formulation of Field Laws: the Cell Method.
- 579 CMES: Comput. Model. Eng. Sci., vol. 2, no. 2, pp. 237–258.
- Tonti, E. (in press): *The Mathematical Structure of Classical and Relativistic Phys- ical Theories*, Springer.
- <sup>582</sup> Wu, J.-Y.; Chang, C.-W. (2011): A Differential Quadrature Method for Multi-<sup>583</sup> Dimensional Inverse Heat Conduction Problem of Heat Source. *CMC: Comput.*
- <sup>584</sup> *Mater. Con.*, vol. 25, no. 3, pp. 215–238.
- **Yeih, W.; Liu, C.-S.; Kuo, C.-L.; Atluri, S.N.** (2010): On solving the direct/inverse
- cauchy problems of laplace equation in a multiply connected domain, using the
- <sup>587</sup> generalized multiple-source-point boundary-collocation Trefftz method & charac-
- teristic lengths. CMC: Comput. Mater. Con., vol. 17, no. 3, pp. 275–302.
- **Zhu, H.H.; Cai, Y.C.; Paik, J.K.; Atluri, S.N.** (2010): Locking-free thick-thin rod/beam element based on a von Karman type nonlinear theory in rotated reference frames for large deformation analyses of space-frame structures. *CMES: Comput.*
- <sup>592</sup> *Model. Eng. Sci.*, vol. 57, no. 2, pp. 175–204.
- <sup>593</sup> Zovatto, L. (2001): Nuovi Orizzonti per il Metodo delle Celle: Proposta per un
- <sup>594</sup> Approccio Meshless. *Proc., AIMETA GIMC* (in Italian), Taormina, Italy, pp. 1–10.

